

4.0.1.1.1-1

uniformly distributed

EFFECT OF REINFORCEMENT

OBJECTIVE

This example illustrates the effect of reinforcement ratio on displacement and stresses in concrete elements.

STRUCTURE

The example consists of two concrete specimens having the dimensions:
 Cross-section - rectangle 100 mm x 100 mm,
 Length - 1000 mm

The samples are supported at the bottom and axially loaded at the top.

INPUT DATA

```

=====
;                               ADAPT-ABI
;                               1733 Woodside Rd # 220, Redwood City, Ca 94061   www.adaptsoft.com
;                               =====
; Name of this file is: 6-2-1a   Date of last update: April 30, 2002
    
```

```

START
TITLE N=1
                Example of effect of reinforcement ratio
    
```

UNITS U=SI

```

CONCRETE PARAMETERS N=1
1 M=ACI a=0 b=1 W=0.0000024
    
```

```

MESH INPUT
NODES N=4
1 Y= 0.00 X=0.0
2 Y=1000.00 X=0.0
3 Y= 0.00 X=2000.0
4 Y=1000.00 X=2000.0
    
```

```

SECTION PROPERTIES N=1
1 B=100 D=100
    
```

```

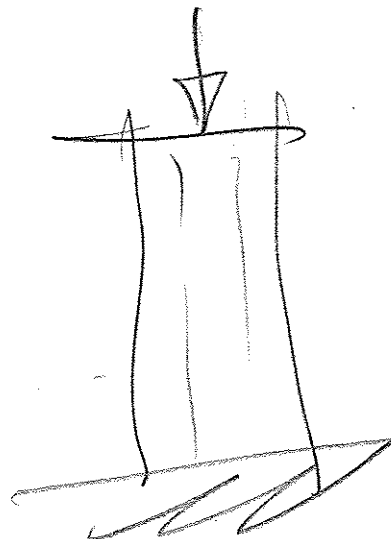
CONCRETE PROPERTIES N=1
1 Fpc=30 Cr=0.0 Sh=0.0 W=0.0 Ac=0.0
    
```

```

MILD STEEL PROPERTIES N=2
1 Es=200000 P=0.01
2 Es=200000 P=0.05
    
```

```

ELEMENTS N=2
FRAME N=2
1,1,2 C=1 X=1 Day=0 St=1
    
```



2,3,4 C=1 X=1 Day=0 St=2

```
MESH COMPLETE
SET G=0,0
CHANGE STRUCTURE
  BUILD N=1,2,1
  RESTRAINTS
    1 R=1,1,1
    3 R=1,1,1
CHANGE COMPLETE
SOLVE Day=28      ! OUTPUT
LOADING
  N=2 F=0,-50000,0
  N=4 F=0,-50000,0
SOLVE Day=28      ! OUTPUT
STOP
```

RESULTS

The verification is performed at Day=28.

Hand calculated results are as follows:

Loading force $F=50$ kN

Cross-section area $A=100\text{mm} \times 100\text{mm} = 10000\text{mm}^2$

Concrete Modulus of Elasticity:

$F'c = 30$ MPa

$E_c = 1.3518 \times 10^{12} \times (W)^{1.5} \times (F'c)^{0.5} = 1.3518 \times 10^{12} \times (2.4 \times 10^{-6})^{1.5} \times (30)^{0.5}$

$E_c = 27529$ MPa

Steel/Concrete Modulus Ratio

$N = E_s/E_c = 200000/27529 = 7.265$

Calculations for Specimen 1. ($P=0.01$)

Stress in concrete

$\sigma = (F/A)/(1+n*P) = (50000/10000)/(1+7.265*0.01) = 4.661\text{ N/mm}^2$

Program calculated value $\sigma = 4.661\text{ N/mm}^2$

Displacement

$\delta = (F*L)/(E_c*A)/(1+n*P) = (50000*1000)/(27529*10000)/(1+7.265*0.01)$

$\delta = 0.169325\text{ mm}$

Program calculated value $\delta = 0.16933\text{ mm}$

Calculations for Specimen 2. ($P=0.05$)

Stress in concrete

$$\sigma = (F/A)/(1+n*P) = (50000/10000)/(1+7.265*0.05) = 3.6677 \text{ N/mm}^2$$

Program calculated value $\sigma = 3.6677 \text{ N/mm}^2$

Displacement

$$\delta = (F*L)/(Ec*A)/(1+n*P) = (50000*1000)/(27529*10000)/(1+7.265*0.05)$$

$$\delta = 0.13323 \text{ mm}$$

Program calculated value $\delta = 0.13323 \text{ mm}$

Hand calculated values compare well with program output.

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 ADAPT-ABI BASIC Large Size Release 4.06
 ADAPT-ABI for Bridges and Frames

DATE: Jun 21, 2002
 TIME: 10:43:53

1 - PROBLEM TITLE:
 EXAMPLE OF EFFECT OF REINFORCEMENT RATIO

2 - UNITS
 MKS

3 - MATERIALS
 3.1 CONCRETE PROPERTIES

CONCRETE PROPERTIES: N = 1
 CONCRETE NO. 1
 MODEL NO. 1
 ULTIMATE STRENGTH 3.000E+02
 CREEP COEFF /SCALE 0.000E+00
 SHRINK STRAIN/SCALE 0.000E+00
 UNIT WEIGHT 0.000E+00
 THERM EXPN COEFF 0.000E+00

3.2 MILD STEEL PROPERTIES
 N = 2
 MILD STEEL NO. ELASTIC MODULUS PERCENTAGE IN CROSS SECTION THERMAL EXPANSION COEFFICIENT
 1 2.00000E+06 1.00000E+00 0.00000E+00
 2 2.00000E+06 5.00000E+00 0.00000E+00

4 - SECTION GEOMETRIES

4.1 INPUT OR COMPUTED SECTION PROPERTIES
 N = 1

SECTION NO. 1
 CROSS SECTION AREA 1.000E+02
 MOMENT OF INERTIA 8.333E+02
 DISTANCE CG TO TOP 5.000E+00
 DISTANCE CG TO BOT 5.000E+00
 SHRIN FACTOR, TOP 1.000E+00
 SHRIN FACTOR, BOT 1.000E+00

5 - FRAME GEOMETRY

5.1 NODES
 N = 4

NODE	X-COORD	Y-COORD	NODE	X-COORD	Y-COORD
1	.000	.000	3	200.000	.000
2	.000	100.000	4	200.000	100.000

5.2 FRAME ELEMENTS

5.2.1 PRIMARY FRAME ELEMENTS
 N = 2

ELEMENT	NODE	CONCR	STEEL	SECT	CASTING

NO.	I	J	TYPE	TYPE	DAY
1	1	2	1	1	0
2	3	4	1	2	1

CONSTRUCTION AND SOLUTION AT DAY 28 STAGE 1

100 - SOLUTION CONTROL DATA

CURRENT TEMPERATURE..... 20.00
 X-DIRECTION GRAVITY MULTIPLIER .00
 Y-DIRECTION GRAVITY MULTIPLIER .00
 STRESS CONVERGENCE FACTOR..... .70

102 - STRUCTURE

102.1 ACTIVE NODES

1 2 3 4

102.2 ACTIVE FRAME ELEMENTS

1 2

105 - NODAL BOUNDARY CONDITIONS AND TOTAL DISPLACEMENTS

Legend: 0 = Free ; 1 = Fixed

NODE	U(X)	U(Y)	R(Z)	X-DISP	Y-DISP	Z-DISP
1	1	1	1	0.0000E+00	0.0000E+00	0.0000E+00
2	0	0	0	0.0000E+00	0.0000E+00	0.0000E+00
3	1	1	1	0.0000E+00	0.0000E+00	0.0000E+00
4	0	0	0	0.0000E+00	0.0000E+00	0.0000E+00

106 - TOTAL REACTIONS AT FIXED NODES

NODE	X-FORCE	Y-FORCE	Z-MOMENT
1	0.0000E+00	0.0000E+00	0.0000E+00
3	0.0000E+00	0.0000E+00	0.0000E+00
TOTAL	0.0000E+00	0.0000E+00	0.0000E+00

107 - FRAME ELEMENT ACTIONS

107.1 PRIMARY ELEMENTS

ELEMENT	BENDING (END I)	BENDING (END J)	SHEAR FORCE	AXIAL FORCE
1	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
2	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00

108 - STRESSES

ELEMENT	I-TOP	I-BOT	J-TOP	J-BOT	AXIAL-I	AXIAL-J
1	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
2	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00

CONSTRUCTION AND SOLUTION AT DAY 28 STAGE 2

100 - SOLUTION CONTROL DATA

CURRENT TEMPERATURE..... 20.00
 X-DIRECTION GRAVITY MULTIPLIER .00
 Y-DIRECTION GRAVITY MULTIPLIER .00
 STRESS CONVERGENCE FACTOR..... .70

2 0.0000E+00 0.0000E+00 0.0000E+00 -5.0000E+03

108 - STRESSES

ELEMENT I-TOP I-BOT J-TOP J-BOT AXIAL-I AXIAL-J
1 -4.6644E+01 -4.6644E+01 -4.6644E+01 -4.6644E+01 -4.6644E+01 -4.6644E+01
2 -3.6770E+01 -3.6770E+01 -3.6770E+01 -3.6770E+01 -3.6770E+01 -3.6770E+01

102 - STRUCTURE

102.1 ACTIVE NODES

1 2 3 4

102.2 ACTIVE FRAME ELEMENTS

1 2

104 - LOADING

104.1 EXTERNALLY APPLIED LOAD OF THIS INCREMENT

NODE X-FORC Y-FORC Z-MOMT X-DISP Y-DISP Z-ROTN
2 0.0000E+00 -5.0000E+03 0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00
4 0.0000E+00 -5.0000E+03 0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00

104.2 ELEMENT TEMPERATURES APPLIED AT THIS INCREMENT

ELEMENT TEMPERATURES

FRAME TOP FIBER BOTTOM FIBER
ELEMENT TEMPERATURE TEMPERATURE

1 20.0 20.0
2 20.0 20.0

104.3 TOTAL OF EXTERNALLY APPLIED LOADING AT THIS STAGE

NODE X-FORC Y-FORC Z-MOMT X-DISP Y-DISP Z-ROTN
2 0.0000E+00 -5.0000E+03 0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00
4 0.0000E+00 -5.0000E+03 0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00

104.4 TOTAL OF ELEMENT TEMPERATURES AT THIS STAGE

ELEMENT TEMPERATURES

FRAME TOP FIBER BOTTOM FIBER
ELEMENT TEMPERATURE TEMPERATURE

1 20.0 20.0
2 20.0 20.0

105 - NODAL BOUNDARY CONDITIONS AND TOTAL DISPLACEMENTS

Legend: 0 = Free ; 1 = Fixed

NODE U(X) U(Y) R(Z) X-DISP Y-DISP Z-ROTN
1 1 1 1 0.0000E+00 0.0000E+00 0.0000E+00
2 0 0 0 0.0000E+00 -1.6782E-02 0.0000E+00
3 1 1 1 0.0000E+00 0.0000E+00 0.0000E+00
4 0 0 0 0.0000E+00 -1.3230E-02 0.0000E+00

106 - TOTAL REACTIONS AT FIXED NODES

NODE X-FORCE Y-FORCE Z-MOMENT
1 0.0000E+00 -5.0000E+03 0.0000E+00
3 0.0000E+00 -5.0000E+03 0.0000E+00

TOTAL 0.0000E+00 -1.0000E+04 0.0000E+00

107 - FRAME ELEMENT ACTIONS

107.1 PRIMARY ELEMENTS

ELEMENT BENDING BENDING SHEAR AXIAL
NO (END I) (END J) FORCE FORCE
1 0.0000E+00 0.0000E+00 0.0000E+00 -5.0000E+03